

2-D FILTER DESIGN

TYPES

- *Finite Impulse Response (FIR) – described here*
- *Infinite Impulse Response (IIR) – not discussed*

2-D FILTER DESIGN

ZERO-PHASE FILTERS

- ***$h(m,n)$ is zero-phase if $H(k, l) = H^*(k, l)$, i.e. H is real***
- ***Zero-phase desired in digital filters to avoid signal distortion***

Zero-phase not guaranteed in physical filters, e.g. optical defocus and square scan spots (see Notes 4 and 5)

- ***H real implies***

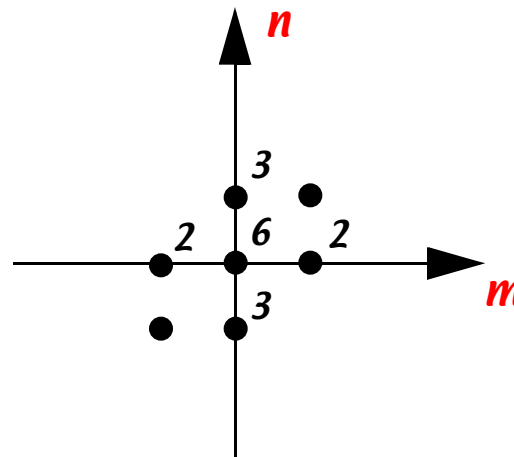
$$h(m, n) = h^*(-m, -n)$$

Prove the above equation

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- Furthermore, since h is assumed real in our case,

$h(m, n) = h(-m, -n)$, i.e. h is **two-fold** symmetric

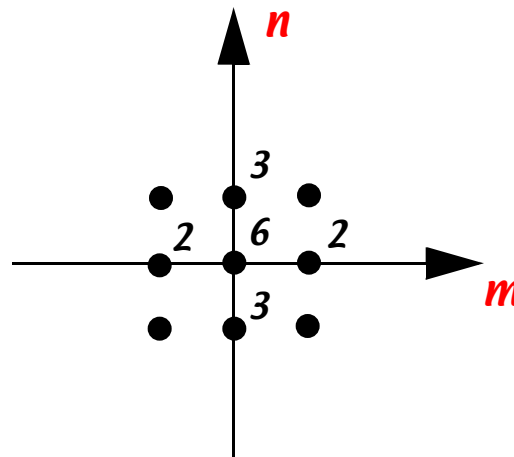


- Greater symmetry reduces number of independent points (Degrees of Freedom (DOF)) required in filter design

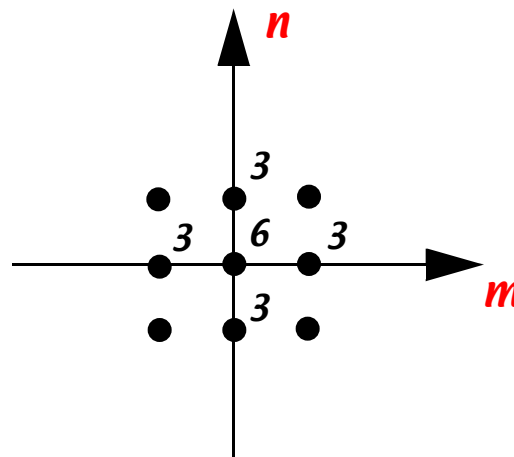
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- **Additional symmetries**

four-fold (includes two-fold): $h(m, n) = h(-m, n) = h(m, -n)$



eight-fold (includes four-fold): $h(m, n) = h(-m, n) = h(m, -n) = h(n, m)$



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FILTER SPECIFICATION

- Frequency domain
- Ideal, continuous, radial filters (note, none are FIR)

type	$F(\omega)$	$f(r)$
Low-Pass Filter (LPF)	$\text{cyl} \frac{r}{2_c}$	$\frac{1}{4} \text{somb}(2_c r)$
High-Pass Filter (HPF)	$1 - \text{cyl} \frac{r}{2_c}$	$\frac{(r)}{r} - \frac{1}{4} \text{somb}(2_c r)$
Band-Pass Filter (BPF)	$\text{cyl} \frac{r}{2_2} - \text{cyl} \frac{r}{2_1}, \quad 2_2 > 2_1$	$\frac{1}{4} [\text{somb}(2_2 r) - \text{somb}(2_1 r)]$
Band-Stop Filter (BSF)	$1 - \text{cyl} \frac{r}{2_2} + \text{cyl} \frac{r}{2_1}, \quad 2_2 > 2_1$	$\frac{(r)}{r} - \frac{1}{4} [\text{somb}(2_2 r) - \text{somb}(2_1 r)]$

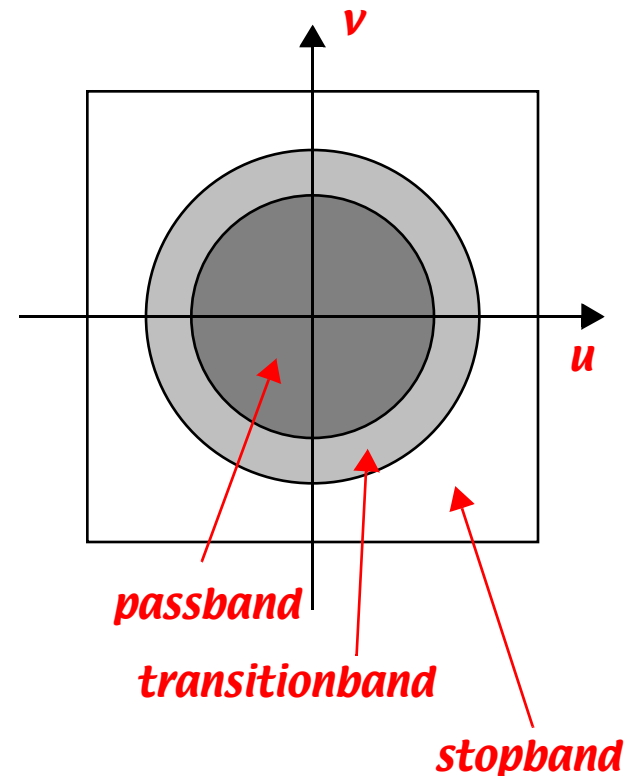
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- *Amplitude transition cannot be sharp with real filters*
- *Therefore, specify transition region and **tolerances** in designed filters*

in passband region: $1 - \epsilon_p < |H(u, v)| < 1 + \epsilon_p$

in stopband region: $|H(u, v)| < \epsilon_s$

which measure quality of filter relative to ideal case



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FILTER DESIGN

- Assume a continuous, periodic frequency domain filter and a discrete spatial domain filter, with the **Discrete-Space Fourier Transform** relation,

$$H(u, v) = \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} h(m, n) e^{-j2\pi um} e^{-j2\pi vn}$$
$$h(m, n) = \int_{u=-1/2}^{1/2} \int_{v=-1/2}^{1/2} H(u, v) e^{j2\pi um} e^{j2\pi vn} du dv$$

Rewrite in terms of angular frequencies $\omega_1 = 2\pi u$, $\omega_2 = 2\pi v$

Examples

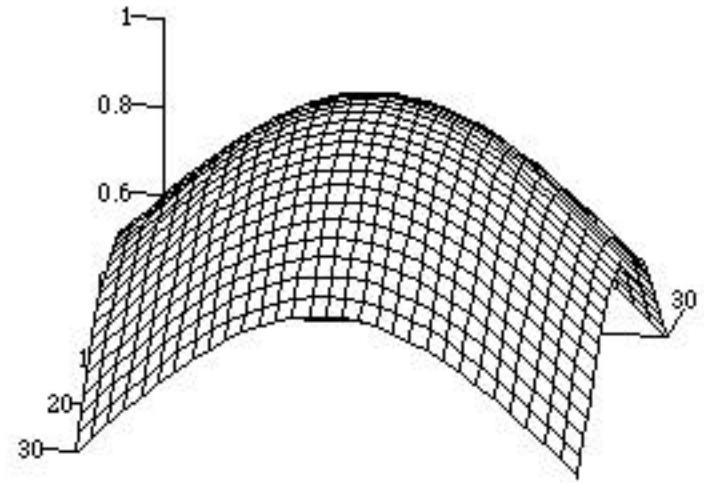
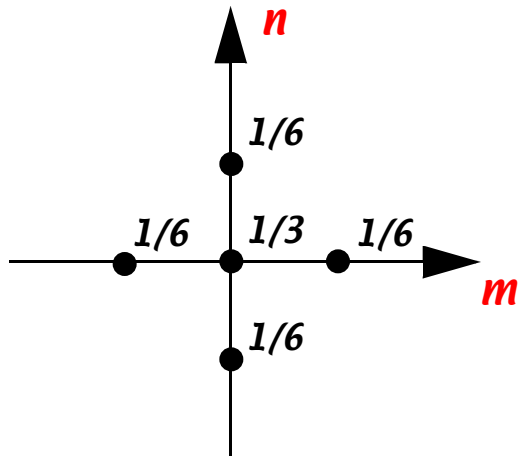
- Specify H and calculate h

$$H(u, v) = \text{rect} \left(\frac{u}{a}, \frac{v}{b} \right), |u| < 1/2, |v| < 1/2$$

$$h(m, n) = |a||b| \text{sinc}(am, bn)$$

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- Specify h and calculate H



$$\begin{aligned} H(u, v) &= \sum_{m=-1}^1 \sum_{n=-1}^1 h(m, n) e^{-j2\pi um} e^{-j2\pi vn} \\ &= \frac{1}{3} + \frac{1}{6} (e^{-ju} + e^{ju} + e^{-jv} + e^{jv}) \\ &= \frac{1}{3} + \frac{1}{6} (2\cos u + 2\cos v) \\ &= \frac{1}{3} (1 + \cos u + \cos v) \end{aligned}$$

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Methods for Filter Design

- *window (1-D extension)*
- *frequency sampling (1-D extension)*
- *transformation (unique to 2-D)*

2-D FILTER DESIGN

Window Method

- Assume a **desired** frequency response $H_d(u, v)$
- Ideal frequency domain filters result in Infinite Impulse Responses (IIR)
- Limit the extent of the spatial response with a **window function w**

$$h(m, n) = h_d(m, n)w(m, n)$$

- Corresponds to a convolution in frequency domain

$$H(u, v) = H_d(u, v) \cdot W(u, v)$$

- **Desirable properties of $W(u, v)$:**
 - narrow main-lobe
 - low side-lobes
 - finite extent in spatial domain

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Generation of 2-D windows from 1-D windows

- **Two ways:**

Implement 1-D window functions in separable 2-D window

$$w(m, n) = w_1(m)w_2(n)$$

$$W(u, v) = W_1(u)W_2(v)$$

Rotate 1-D window about the origin as “generating function” to create 2-D radial (circularly symmetric) function (see Notes2)

$$w(m, n) = w(\sqrt{m^2 + n^2})$$

$$W(u, v) = W(\sqrt{u^2 + v^2})$$

2-D FILTER DESIGN

- **Examples**

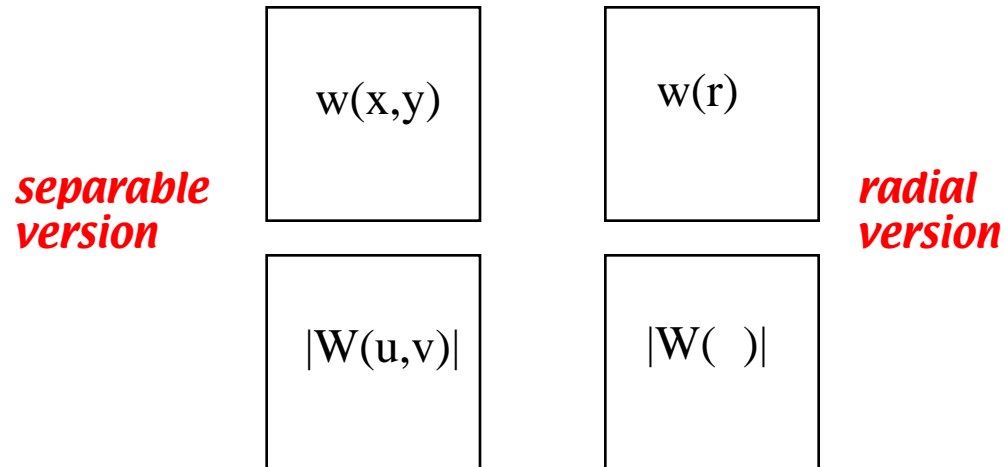
- **All defined with:**

width $b=8$

plot array $M=N=32$

spatial region of support = 8×8 (separable) or radius = 4 (radial)

plot layout:

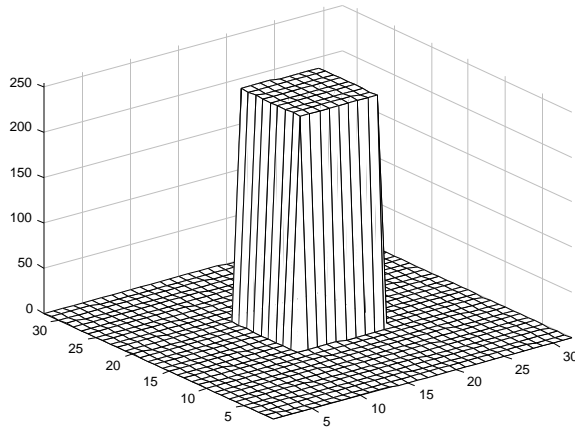


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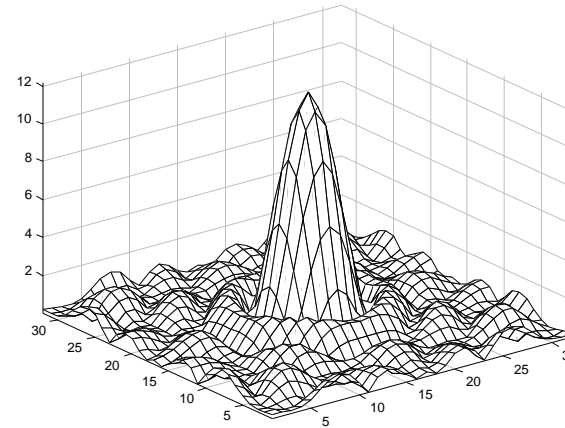
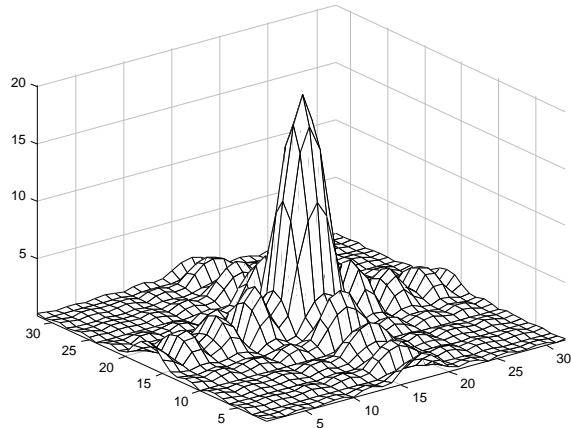
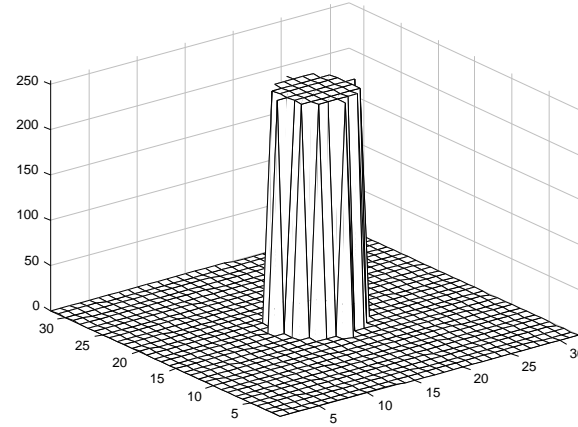
- **rectangle** $w(x) = 1$ (see Notes1)

- **cylinder** $w(r) = cyl \frac{r}{b}$

rectangle window - separable version

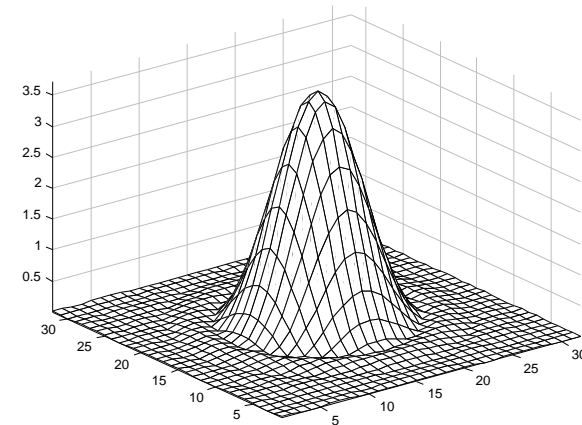
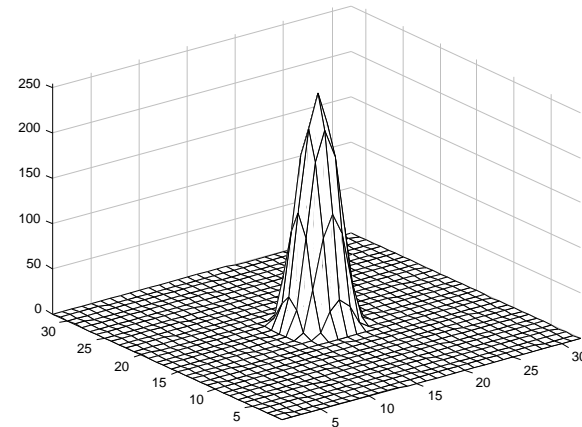


radial version



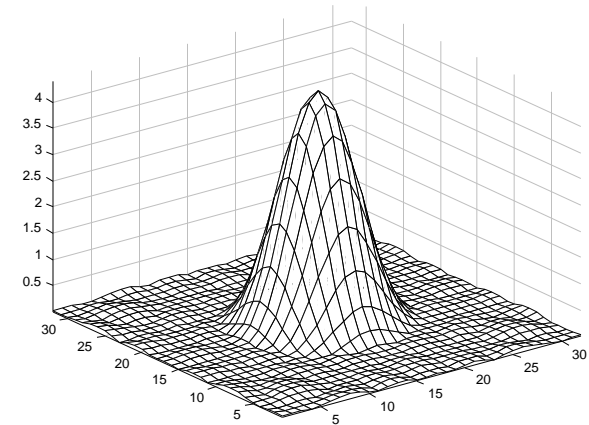
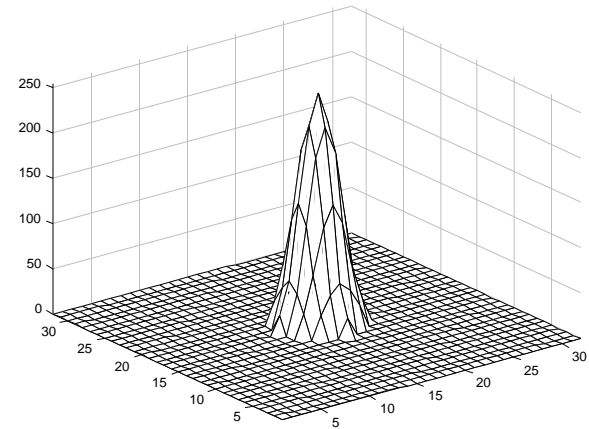
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- **Hanning (raised cosine)** $w(r) = 0.5 + 0.5 \cos 2 \frac{r}{b}$



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- **Hamming** $w(r) = 0.54 + 0.46 \cos 2 \frac{r}{b}$

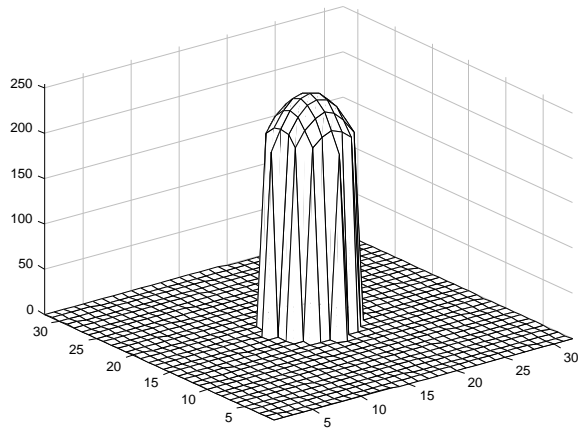


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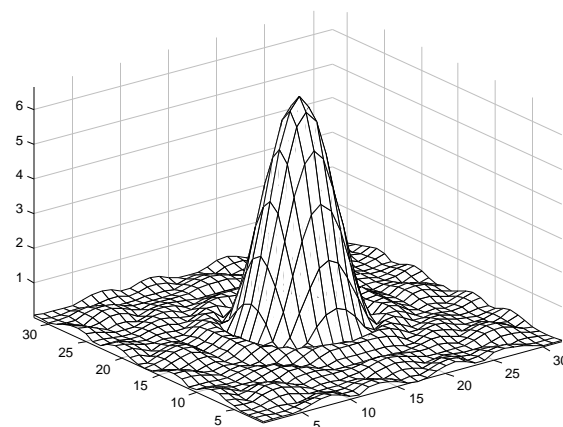
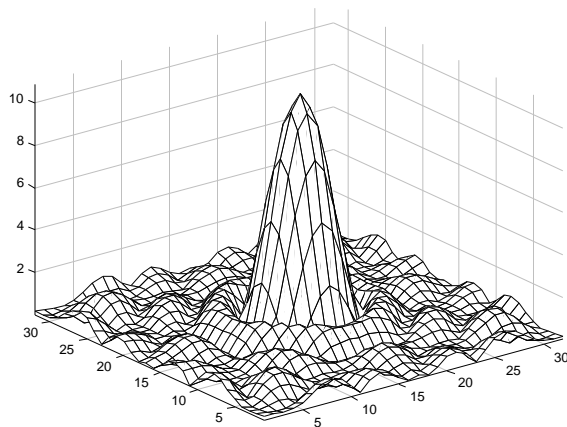
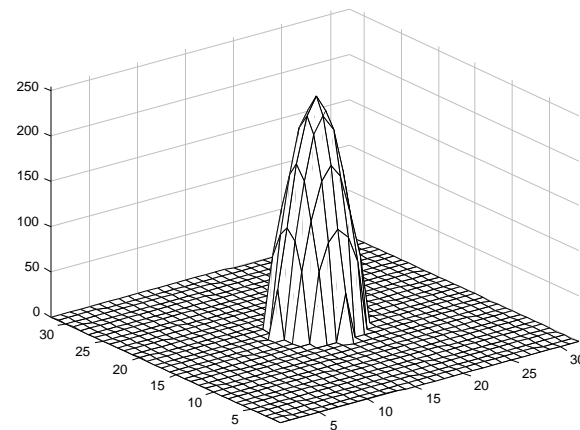
- **Kaiser** $w(r) = \frac{1}{I_0(\beta)} I_0(\beta \sqrt{1 - (2r/b)^2})$

where I_0 is a modified Bessel function of the first kind, order zero, and β controls the window shape:
smaller \rightarrow mainlobe narrower, larger \rightarrow sidelobes lower

= 1 radial version



= 3



2-D FILTER DESIGN

Frequency Sampling Method

- Sample 2-D continuous frequency domain filter $H(u,v)$ to obtain $H(k,l)$ (origin-centered)
- Calculate inverse DFT to obtain $h(m,n)$ (origin-centered)

Frequency Sampling Method

- add linear phase (M and N odd)

$$H_l(u, v) = H_z(u, v) e^{-j2\pi u((M-1)/2)} e^{-j2\pi v((N-1)/2)}$$

$$H_l(k, l) = H_l(k/M, l/N)$$

- sample $k = 0, 1, \dots, M-1$
 $l = 0, 1, \dots, N-1$

- inverse DFT $h_l(m, n)$

- shift $h_z(m, n) = h_l(m + (M-1)/2, n + (N-1)/2)$

2-D FILTER DESIGN

- *Sampling of ideal frequency domain filters results in discontinuities at cut-off and cut-on frequencies*
- *Apply “smoothing” in transition region*

Simple linear transition works fine

- *Origin-centering important to maintain zero phase*